

Model-Based Controller Design

Linear control design techniques

- Three major steps for control design
 - Modeling, analysis, and design (MAD) process
- The control design is based on system's model (**model-based**)
- The closed-loop system must meet certain design specifications
- Model-based design techniques
 - Cascade lead-lag compensator design
 - Optimal linear quadratic regulator (LQR)
 - Pole placement design
 - Decoupling control of multivariable systems
- SISOTool control design environment

Lead-Lag Compensator Design

Phase-lead compensator

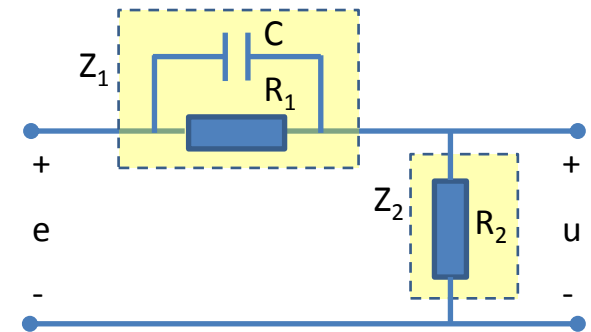
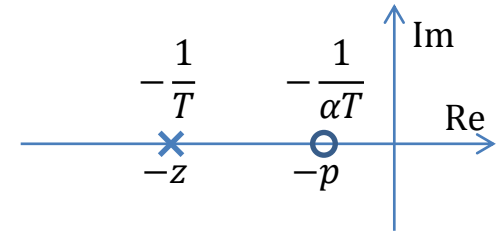
$$G_c(s) = \frac{U(s)}{E(s)} = K \frac{(s+z)}{(s+p)} \quad ; \quad z < p \quad (\text{lead})$$

- Pole on the left side of zero
- Equivalent RC circuit, $K=1$, ($Z_1 = \frac{R_1}{1+R_1Cs}$, $Z_2 = R_2$)

$$G_c(s) = \frac{U(s)}{E(s)} = \frac{Z_2}{Z_1+Z_2} = \frac{1}{\alpha} \frac{(1+\alpha Ts)}{(1+Ts)}$$

$$T = \frac{R_1 R_2}{R_1 + R_2} C, \quad \alpha = \frac{R_1 + R_2}{R_2} > 1$$

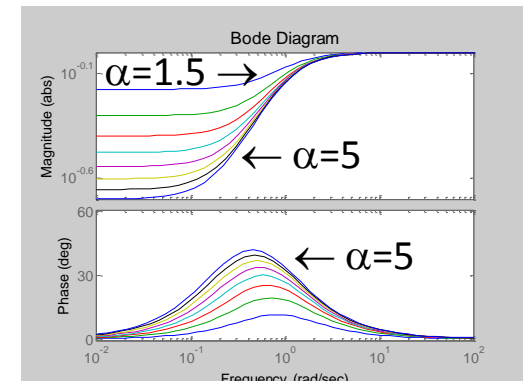
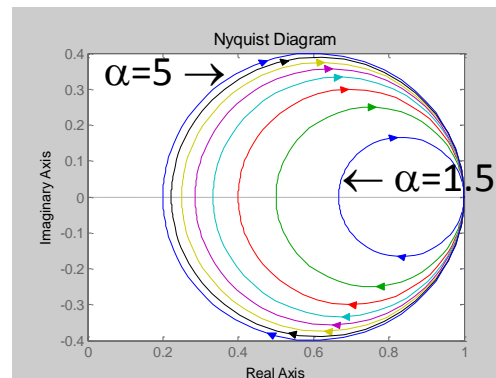
Or: $p = \frac{1}{T}, \quad z = \frac{1}{\alpha T}$



- Bode and Nyquist plots of lead compensator

$$T=1$$

$$\alpha=1.5:0.5:5$$



Lead-Lag Compensator Design

Example (lead compensator):

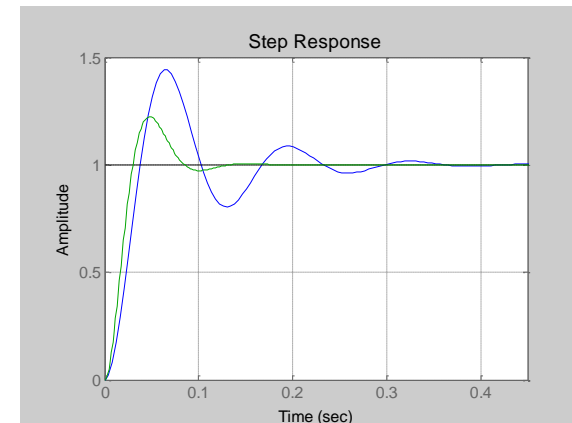
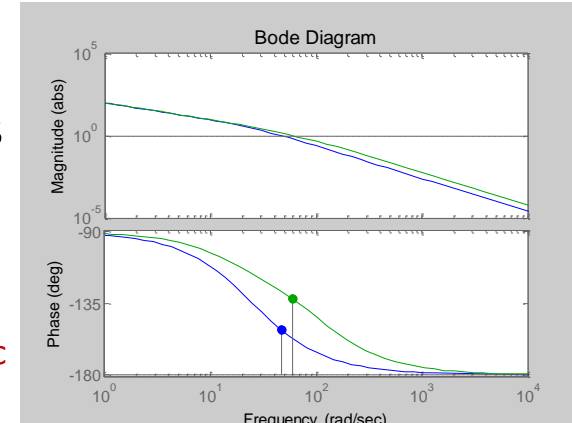
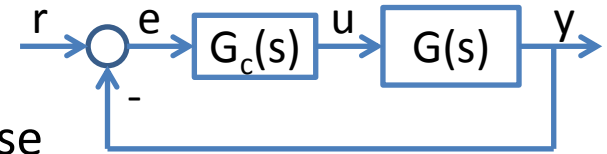
For $G(s) = \frac{100}{s(0.04s+1)}$, increase the closed-loop phase
 Phase margin: PM=28.0243° at $\omega_{cp}=46.9701$ rad/sec

- Consider the lead compensator $G_c(s) = \frac{(1+0.0262s)}{(1+0.0106s)}$
- Draw and compare the Bode plots and step responses

Matlab code:

```
G=tf(100,[0.04,1,0]);
[Gm,Pm,wcg,wcp]=margin(G),
Gc1=tf([0.0262,1],[0.0106,1]); GGc1=G*Gc1;
[Gm1,Pm1,wcg1,wcp1]=margin(GGc1),
figure(1), bode(G,GGc1); grid off;
Gcl=feedback(G,1,-1);
Gcl1=feedback(GGc1,1,-1);
figure(2), step(Gcl,Gcl1);
```

Phase margin with lead
 compensation:
 PM=47.6° at $\omega_{cp}=60.3$ rad/sec



Lead-Lag Compensator Design

Phase-lag compensator

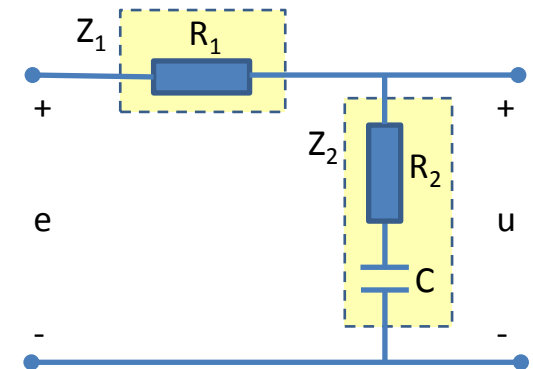
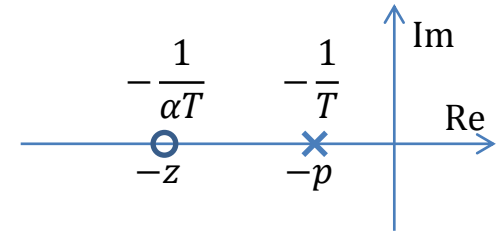
$$G_c(s) = \frac{U(s)}{E(s)} = K \frac{(s+z)}{(s+p)} \quad ; \quad z > p \quad (\text{lag})$$

- zero on the left side of pole
- Equivalent RC circuit, $K=1$, ($Z_1 = R_1$, $Z_2 = R_2 + \frac{1}{Cs}$)

$$G_c(s) = \frac{U(s)}{E(s)} = \frac{Z_2}{Z_1 + Z_2} = \frac{1 + \alpha Ts}{1 + Ts}$$

$$T = (R_1 + R_2)C, \quad \alpha = \frac{R_2}{R_1 + R_2} < 1$$

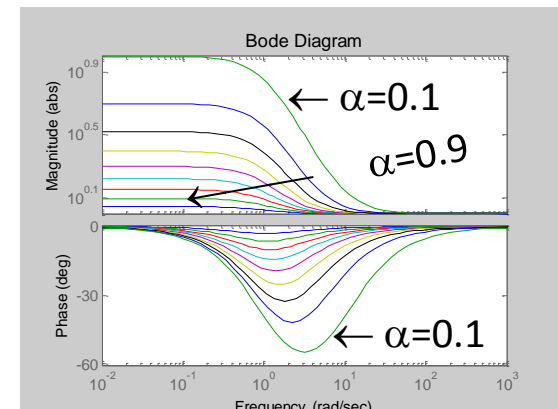
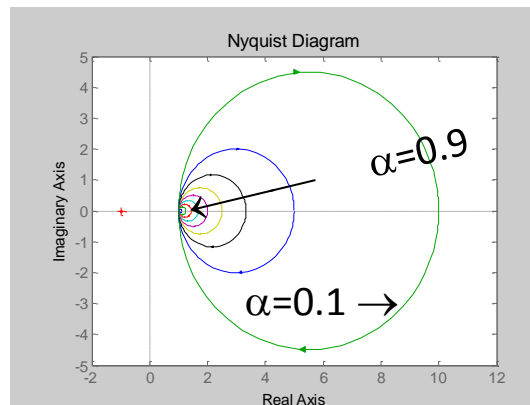
$$\text{Or: } p = \frac{1}{T}, \quad z = \frac{1}{\alpha T}, \quad K = \alpha$$



- Bode and Nyquist plots of lag compensator

$$T=1, K=1$$

$$\alpha=0.9:-0.1:0.1$$



Lead-Lag Compensator Design

Example (lag compensator):

For $G(s) = \frac{100}{s(0.04s+1)}$, increase the closed-loop phase

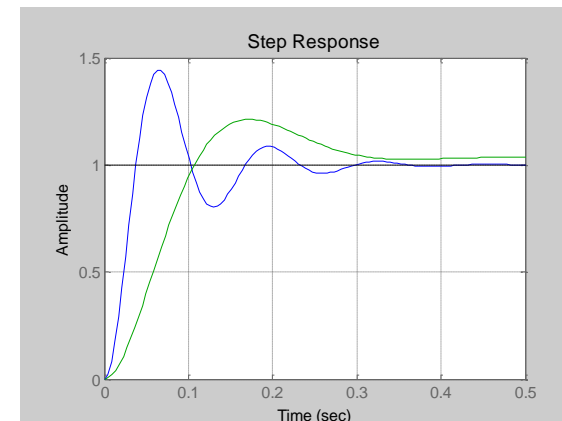
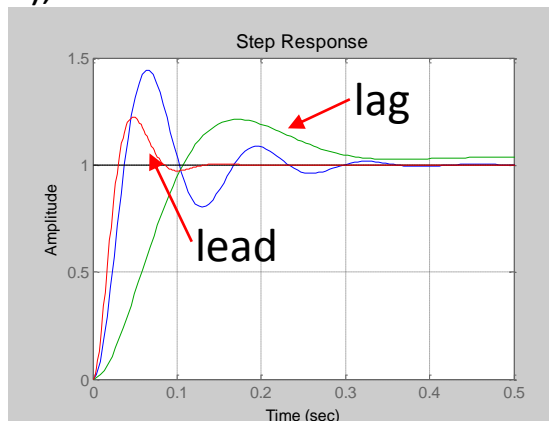
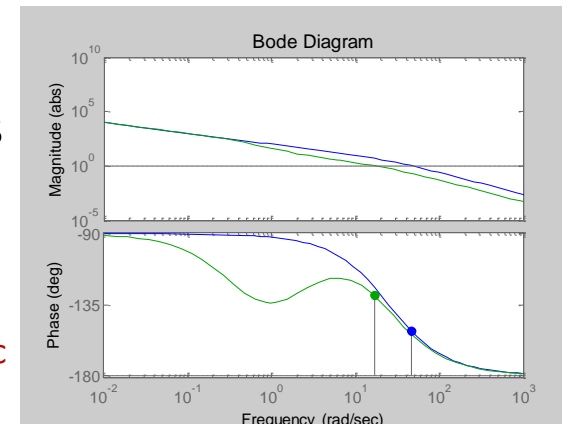
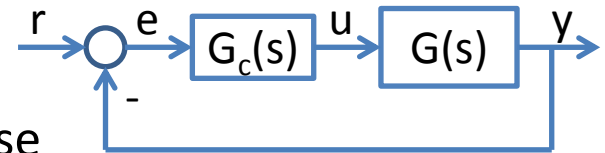
Phase margin: $PM=28.0243^\circ$ at $\omega_{cp}=46.9701$ rad/sec

- Consider the lag compensator $G_c(s) = \frac{(1+0.5s)}{(1+2.5s)}$
- Draw and compare the Bode plots and step responses

Matlab code:

```
G=tf(100,[0.04,1,0]);
[Gm,Pm,wcg,wcp]=margin(G),
Gc2=tf([0.5,1],[2.5,1]); GGc2=G*Gc2;
[Gm2,Pm2,wcg2,wcp2]=margin(GGc2),
figure(1), bode(G,GGc2); grid off;
Gcl=feedback(G,1,-1);
Gcl2=feedback(GGc2,1,-1);
figure(2), step(Gcl,Gcl2);
Gc1=tf([0.0262,1],[0.0106,1]);
GGc1=G*Gc1;
Gcl1=feedback(GGc1,1,-1);
figure(3), step(Gcl,Gcl2,Gcl1);
```

Phase margin with lead
compensation:
 $PM=47.6^\circ$ at $\omega_{cp}=60.3$ rad/sec



Lead-Lag Compensator Design

Phase lead-lag compensator

$$G_c(s) = \frac{U(s)}{E(s)} = K \frac{(s+z_1)(s+z_2)}{(s+p_1)(s+p_2)} ; \quad \begin{array}{l} z_1 < p_1 \text{ (lead)} \\ z_2 > p_2 \text{ (lag)} \end{array}$$

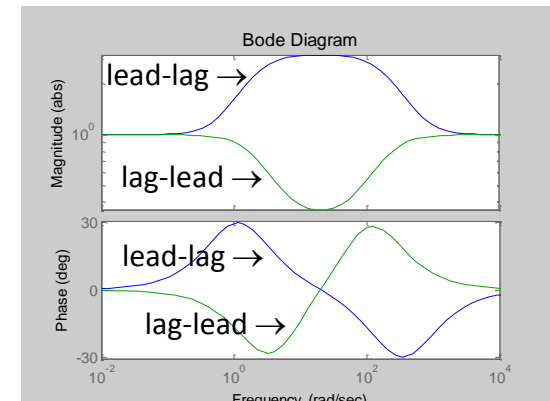
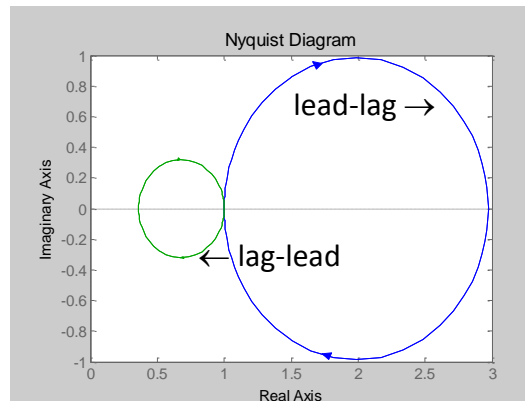
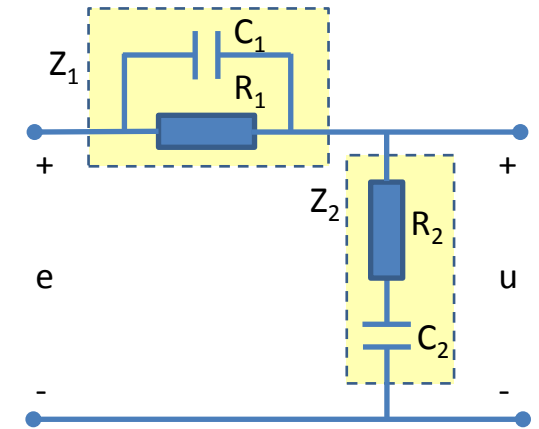
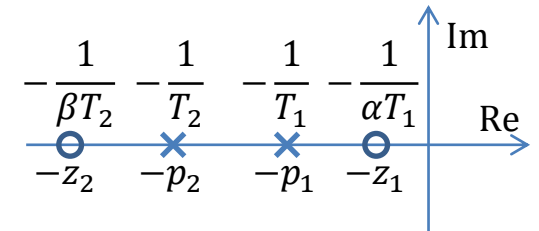
- For lead-lag, (z_1, p_1) is on the left of (z_2, p_2)
- For lag-lead, (z_1, p_1) is on the right of (z_2, p_2)
- Equivalent RC circuit, $(Z_1 = \frac{R_1}{1+R_1C_1s}, Z_2 = R_2 + \frac{1}{C_2s})$

$$G_c(s) = \frac{U(s)}{E(s)} = \frac{Z_2}{Z_1+Z_2} = \frac{(1+\alpha T_1s)(1+\beta T_2s)}{(1+T_1s)(1+T_2s)}$$

$$\alpha T_1 = R_1 C_1, \quad \beta T_2 = R_2 C_2, \quad \alpha\beta = 1 \quad \alpha > 1, \quad \beta < 1$$

$$T_1 + T_2 = R_1 C_1 + R_2 C_2 + R_1 C_2, \quad T_1 T_2 = R_1 C_1 R_2 C_2$$

- Bode and Nyquist plots of **lead-lag** ($T_1=0.5, T_2=0.005$) and **lag-lead** ($T_2=0.5, T_1=0.005$) compensators with ($\alpha=3, \beta=1/3$)



Lead-Lag Compensator Design

Lead-lag design by phase-margin assignment

Given Plant model: $G(s) = \frac{b_0 s^m + b_1 s^{m-1} + \dots + b_{m-1} s + b_m}{s^v (a_0 s^{n-v} + a_1 s^{n-v-1} + \dots + a_{n-v+1} s + a_{n-v})}$

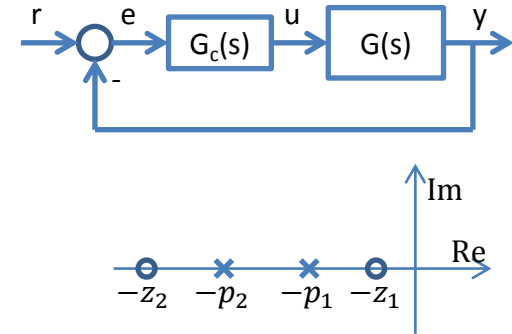
Design compensator: $G_c(s) = K \frac{(s+z_1)(s+z_2)}{(s+p_1)(s+p_2)}$; $z_1 \leq p_1$ (lead) $z_2 \geq p_2$ (lag)

Design specifications:

- Desired cross-over frequency: ω_{cd}
- Desired phase-margin of the compensated system at ω_{cd} : PM_d
- Desired error-constant: greater than or equal to K_{ed}

Denote:

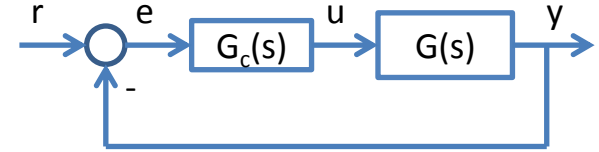
- Error constant: $K_e = \lim_{s \rightarrow 0} s^v G_o(s)$, where v is the number of poles of $G(s)$ at the origin, $G_o(s) = G_c(s)G(s)$
- Phase-angle and magnitude of the plant model at ω_{cd} : $\phi_g(\omega_{cd})$, $A(\omega_{cd})$
- Phase-angle of the compensator at ω_{cd} : $\phi_c(\omega_{cd}) = PM_d - 180 - \phi_g(\omega_{cd})$



Lead-Lag Compensator Design

Lead-lag design procedure

$$\phi_c(\omega_{cd}) = PM_d - 180 - \phi_g(\omega_{cd})$$



Case 1: If $\phi_c(\omega_{cd}) > 0$, a lead compensator is needed as

- a) Let $\alpha = \frac{z_1}{p_1} = \frac{1 - \sin \phi_c}{1 + \sin \phi_c} > 1$, then $z_1 = \sqrt{\alpha} \omega_{cd}$, $p_1 = \frac{z_1}{\alpha} = \frac{\omega_{cd}}{\sqrt{\alpha}}$, $K = \frac{\sqrt{\omega_{cd}^2 + p_1^2}}{\sqrt{\omega_{cd}^2 + z_1^2}} \frac{A(\omega_{cd})}{b_m K z_1}$
- The error-constant of compensated system is: $K_e = \lim_{s \rightarrow 0} s^\nu G_c(s)G(s) = \frac{b_m}{a_{n-\nu}} \frac{K z_1}{p_1}$
 - If $K_e \geq K_{ed}$, lead compensator is sufficient
 - If $K_e < K_{ed}$, need lead-lag compensator

Case 2: If $\phi_c(\omega_{cd}) < 0$, a lag compensator is needed as

- a) Let $K = \frac{1}{A(\omega_{cd})}$, $z_2 = \frac{\omega_{cd}}{\beta}$, $p_2 = \frac{K_e}{K_{ed}} z_2$, where $\beta \in [4, 10]$, $K_e = \lim_{s \rightarrow 0} s^\nu G(s) = \frac{b_m}{a_{n-\nu}} K$

Case 3: After lead compensation design, if error-constant specification is not satisfied ($K_e = \lim_{s \rightarrow 0} s^\nu G_c(s)G(s) < K_{ed}$), a lead-lag compensator is needed, consisting of the above phase-lead design and a phase-lag as

- a) Select z_1 , p_1 , K as in case 1. Then, $z_2 = \frac{\omega_{cd}}{\beta}$, $p_2 = \frac{K_e}{K_{ed}} z_2$, where $\beta \in [4, 10]$,

$$K_e = \lim_{s \rightarrow 0} s^\nu G_o(s) = \frac{b_m}{a_{n-\nu}} \frac{K z_1}{p_1}$$

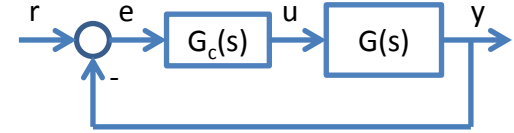
Lead-Lag Compensator Design

Lead-lag design with Matlab

Matlab function: `leadlag()`,

Syntax: `Gc=leadlag(G,wc,PMd,Ke,key)`

- G is the plant model
- w_c is the desired crossover frequency
- PM_d is the desired phase-margin
- K_e is the static error constant
- $key=1,2,3$ for cases 1,2,3
- G_c is the TF of the compensator



Matlab code:

`% Lead-lag compensator design`

```
function Gc=leadlag(G,wc,Gam_c,Kv,key)
G=tf(G); [Gai,Pha]=bode(G,wc); Phi=Gam_c-Pha-180; N=1;
if Phi<0, Ph0=mod(-Phi,70); N0=- (Phi+Ph0)/.70; N=N0+1; end,
Phi_c=Phi*pi/180/N; den=G.den{1}; a=den(length(den):-1:1);
ii=find(abs(a)<=0); num=G.num{1}; G_n=num(end);
if length(ii)>0, a=a(ii(1)+1); else, a=a(1); end; a=abs(a);
alpha=sqrt((1-sin(Phi_c))/(1+sin(Phi_c))); Zc=alpha*wc;
Pc=wc/alpha;
Kc=sqrt(((wc*wc+Pc*Pc)/(wc*wc+Zc*Zc))^N)/Gai;
K1=G_n*Kc*alpha^2/a;
if nargin==4, key=1;
    if Phi_c<0, key=2; else if K1<Kv, key=3; end, end, end
switch key
    case 1, Gc=(tf([1,Zc]*Kc,[1,Pc]))^N;
    case 2, Kc=1/Gai; K1=G_n*Kc/a;
Gc=tf([1,0.1*wc],[1,0.1*K1*wc/Kv]);
    case 3, Zc2=wc*0.1; Pc2=K1*Zc2/Kv; Gcn=Kc*conv(poly(-Zc*ones(N,1)),[1,Zc2]);
        Gcd=conv(poly(-Pc*ones(N,1)),[1,Pc2]); Gc=tf(Gcn,Gcd);
end
```

Lead-Lag Compensator Design

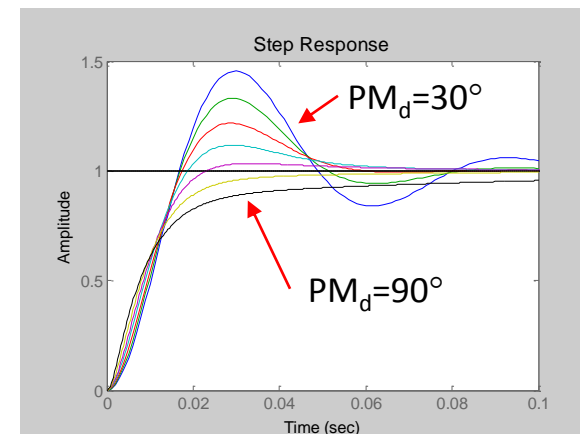
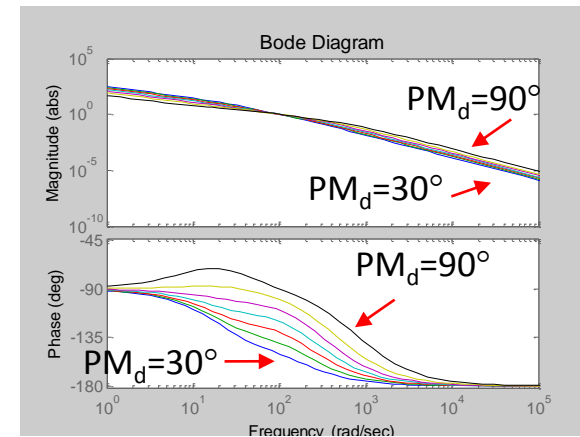
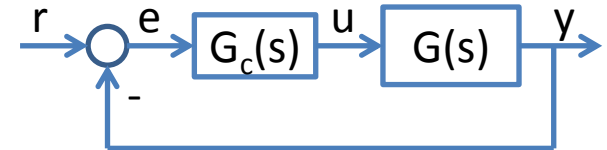
Example:

For $G(s) = \frac{100}{s(0.04s+1)}$, design lead-lag compensator

- Desired phase margin: $PM_d = [30, 40, \dots, 90]^\circ$
- Desired crossover frequency: $\omega_{cd} = 100$ rad/sec
- Desired error constant: $K_{ed} \geq 10$
- Draw and compare the Bode plots and step responses

Matlab code:

```
G=tf(100,[0.04,1,0]); wcd=100; Ked=10;
for pmd=[30,40,50,60,70,80,90],
    Gc=leadlag(G,wcd,pmd,Ked);
    Go=Gc*G; Gcl=feedback(Go,1);
    figure(1), bode(Go); hold on; grid off;
    figure(2), step(Gcl,0.1); hold on; grid off;
end
```



Lead-Lag Compensator Design

Example:

Plant model: $G(s) = \frac{100}{s(s+1)(0.0125s+1)}$

- Design **lead-lag** compensator
 - Desired phase margin: $PM_d = [30, 40, 50, 60, 70, 80, 90]^\circ$
 - Desired crossover frequency: $\omega_{cd} = 50$ rad/sec
 - Desired error constant: $K_{ed} \geq 10$
- Draw and compare the Bode plots and step responses

Matlab code:

```
close all; clear all; clc;
s=zpk('s'); G=100/(s*(s+1)*(0.0125*s+1));
wcd=50; Ked=10;
for pmd=[30,40,50,60,70,80,90],
    Gc=leadlag(G,wcd,pmd,Ked);
    Go=Gc*G; Gcl=feedback(Go,1);
    figure(1), bode(Go); grid off; hold on;
    figure(2), nyquist(Go); grid off; hold on;
    figure(3), nichols(Go); grid off; hold on;
    figure(4), step(Gcl,0.3); grid off; hold on;
end
```

Note: Bad specs → Bad designs

